

A comparison of canal centering abilities of four root canal instrument systems using X-ray micro-computed tomography

Hye-Suk Ko, Heyon-Mee You, Dong-Sung Park*

Department of Conservative Dentistry, Samsung Medical Center, Sungkyunkwan University School of Medicine

ABSTRACT

The purpose of this study was to compare the centering abilities of four root canal instrument systems and the amounts of dentin removed after root canal shaping using them.

The mesial canals of twenty extracted mandibular first molars having 10 - 20° curvature were scanned using X-ray micro-computed tomography (XMCT)-scanner before root canals were instrumented. They were divided into four groups (n = 10 per group). In Group 1, root canals were instrumented by the step-back technique with stainless steel K-Flexofile after coronal flaring. The remainders were instrumented by the crown-down technique with Profile (Group 2), ProTaper (Group 3) or K3 system (Group 4). All canals were prepared up to size 25 at the end-point of preparation and scanned again. Scanned images were processed to reconstruct three-dimensional images using three-dimensional image software and the changes of total canal volume were measured. Pre- and post-operative cross-sectional images of 1, 3, 5, and 7 mm from the apical foramen were compared. For each level, centering ratio were calculated using Adobe Photoshop 6.0 and image software program.

ProTaper and K3 systems have a tendency to remove more dentin than the other file systems. In all groups, the lowest value of centering ratio at 3 mm level was observed. And except at 3 mm level, ProTaper system made canals less centered than the other systems ($p < 0.05$). [J Kor Acad Cons Dent 32(1):61-68, 2007]

Key words: X-ray micro-computed tomography, ProFile, Protaper, K3, Centering ratio, Three dimensional image software

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I . Introduction

Cleaning and shaping of the root canals is the single most important phase of endodontic treatment¹⁾. Canals which seem straight on diagnostic roentgenograms often curve into or out of the flat plane of the film. Teeth with canals that visibly curve mesially or distally often have additional

* Corresponding Author: **Dong-Sung Park**

Department of Conservative Dentistry,
Samsung Medical Center,
50 Ilwon-Dong, Kangnam-Ku, Seoul, Korea, 135-710
Tel: 82-2-3410-2429 Fax: 82-2-3410-0038
E-mail: dsparkh@smc.samsung.co.kr

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curves not apparent in many planes, and these curvatures should be maintained generally as canal preparation progresses¹⁾.

Transportation of the canal in the apical, middle, and coronal thirds has been shown to occur with various instrumentation methods²⁾. However, cleaning and shaping of narrow and curved canals with stainless steel instruments can be difficult and may not provide the optimal shape³⁾.

Shape memory and superelasticity are the main reasons why NiTi alloys have succeeded in endodontics. Files made from Ni-Ti alloy (Nitinol files) in size #15 had two to three times more elastic flexibility in bending and torsion compared with #15 stainless steel files manufactured by the same process, in which the fluted cross-sectional shape was machined directly on the wire blank and suggested that Nitinol endodontic files might be promising for the clinical preparation of curved root canals⁴⁾. It was reported that there was significantly less transportation of the root canal toward the furcation, and less thinning of the root structure with a Ni-Ti rotary instrument (GT files) compared to stainless steel files in the mid-root sections⁵⁾. A Ni-Ti rotary instrument (Hero 642) transported canals less, especially at the middle and coronal thirds of the root canals than stainless steel K-files⁶⁾.

Contemporary available modern NiTi rotary files have unique design properties in terms of cross-sectional geometry. One recent innovation in Ni-Ti rotary instruments is the use of a radial land relief in combination with a positive rake angle in the K3 system. Another active file design was recently introduced as ProTaper, a convex triangular cross-sectional design with an advanced flute design that combines multiple tapers within the shaft.

The purpose of this study was to compare the centering abilities of stainless-steel hand instrument (K-Flexofile) and Ni-Ti rotary instruments (ProFile, ProTaper, K3 systems) and evaluate the amounts of dentin removed after final instrumentation using high-resolution X-ray micro-computed tomography (XMCT) and image software programs.

II. Materials and methods

1. Preparation of specimens

Twenty mandibular molars were selected from fresh extracted teeth without any defect stored in saline solution until used. According to the Schneider's method⁷⁾, the teeth with 10 - 20° mesial root curvature were chosen. The occlusal surface was ground flat, perpendicular to the long axis of the tooth using diamond disc. The vertical groove was formed on distal root surface near the pulp chamber as a reference point for XMCT analysis.

2. Initial XMCT scanning

Specimens were scanned using XMCT scanner (Skyscan 1072, Skyscan b.v.b.a., Aartselaar, Belgium) at 50 μ m interval from the level of working length to the bifurcation area before instrumentation. Approximately 300 cross-sectional images were obtained for each specimen.

3. Root canal preparation

Specimens were randomly divided into four groups (n = 10 canals per group) and prepared using (1) stainless steel K-Flexofile (KF) (Dentsply-Maillefer, Ballaigues, Switzerland) (2) ProFile (PF) system (Dentsply-Maillefer, Ballaigues, Switzerland), (3) ProTaper (PT) system (Dentsply-Maillefer, Ballaigues, Switzerland), and (4) K3 system (SybronEndo, Orange, CA, USA). Size 10 K-Flexofiles were inserted into the mesial canals so that their tips were just visible at the apical foramina, which were separate for both canals. Individual working lengths (WL) were calculated 0.5 mm short of these positions. All canals were prepared up to size 25 at the end-point of preparation. The canals were irrigated between each file with 2.5% sodium hypochlorite. Root canal preparation was done by one operator. All Ni-Ti rotary instruments were rotated at a pre-set r.p.m. and torque following the manufacturer's recommendation using a Tecnika Vision

(Dentsply-Maillefer, Ballaigues, Switzerland).

Canal shaping was done as follows:

Group 1 (KF): The coronal part of the canal was flared with Gates-Glidden burs (Dentsply-Maillefer, Ballaigues, Switzerland) from sizes 1 to 3. Each bur was carried passively into the root canal. A size 25 K-file was instrumented to a point of working length. Files were then stepped back in 1mm increments to size 40.

Group 2 (PF): The canals were prepared in a crown-down fashion using ProFile .04 instruments and/or ProFile .06 instruments. A size 25/.04 or .06 ProFile was introduced one half to two thirds of the way down the canal. The instrument was withdrawn when resistance was felt and was followed by a size 30/.04 or .06 ProFile to approximately the same length. A size 20/.04 or .06 ProFile was then used two thirds to three quarters of the way down the canal, and then a size 15/.04 or .06 ProFile

was used to the WL. After a size 15/.04 or .06 ProFile reached the WL, a size 20/.04 or .06 ProFile was used to the WL in the same manner. The final apical file size was ProFile 25/.06 instrument.

Group 3 (PT): The canals were enlarged with S1 and S2 used in a gentle pumping and brushing action to the WL. Thereafter, F1 and F2 were used to the WL. The final apical size was F2 file.

Group 4 (K3): First, the canals were prepared in a crown-down fashion using K3 .10 and .08 instruments as orifice openers in the coronal third. Second, K3 40/.06 and 35/.06 instruments were used in the middle third. And last K3 30/.06, 25/.06 and 20/.06 were used in the apical third until true working length was reached. The final apical size was K3 25/.06 instrument.

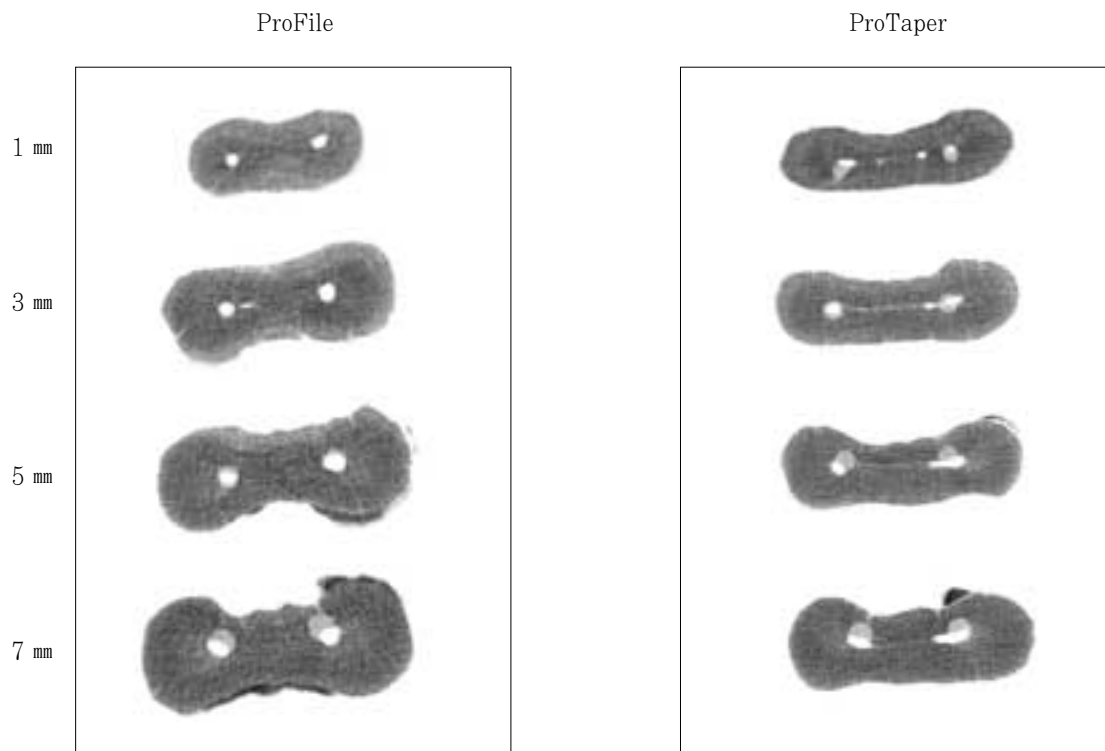


Figure 1. Examples of superimposed images.

Dark gray: Cross section of root after canal shaping

Light gray: Cross section of root before canal shaping

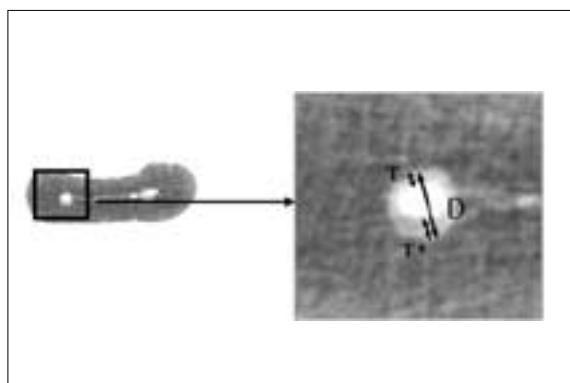


Figure 2. The drawing representing superimposed image of pre- and post-instrumentation canal shapes for measurement of centering ratio.

4. Final XMCT scanning

After root canal preparation, all specimens were scanned using XMCT in the same manner as mentioned above.

5. Measurements and evaluations

All scanned images were processed to reconstruct three-dimensional images using three-dimensional image software (V-works 4.0, Cybermed Inc., Seoul, Korea) and the changes of canal volume were measured. And then, pre- and post-operative cross-sectional images of 1, 3, 5, and 7 mm from the apical foramen were compared (Figure 1). For each level, centering ratio was determined. Centering ratio, reported by Calhoun and Montgomery⁸⁾, was calculated by the following formula: $(T' - T)/D$. T' represents the maximum extent of canal movement in one direction and T is the movement in the opposite direction. D is the diameter of the final canal preparation (Figure 2). To obtain these values, pre- and post-operative images were painted with different color and then two images were superimposed after adjusting the opacity of these images using Adobe Photoshop 6.0 (Adobe Systems Incorporated, San Jose, CA, USA). Centering ratio was calculated by image software program (SigmaScan Pro 5.0, Systat Software Inc., Richmond, CA, USA). The data were analyzed by the one-way ANOVA and

T' : Maximum extent of canal movement in one direction

T : Movement in the opposite direction

D : Diameter of the final canal preparation

Table 1. Mean change of total canal volume (mm^3)

	Mean \pm SD
Group 1 (KF)	0.61 ± 0.33^a
Group 2 (PF)	0.75 ± 0.18^a
Group 3 (PT)	1.34 ± 0.27^b
Group 4 (K3)	1.42 ± 0.17^b

^{a,b}: Groups identified by different alphabets are significantly different ($p < 0.05$).

Groups identified by some alphabets are not significantly different ($p > 0.05$).

Scheffé's multiple range tests at 95% significant level using a statistical software SAS (SAS Enterprise Guide 3.0, Cary, NC, USA).

III. Results

Change of canal volume

The amount of dentin removed following instrumentation was calculated. Group 3 (PT) and Group 4 (K3) have a tendency to remove more dentin than other file systems. The amount of canal volume change was least in Group 1 (KF), followed in increasing order by Group 2 (PF), Group 3 (PT), and Group 4 (K3). There was no significant difference between Group 3 (PT) and Group 4 (K3) ($p > 0.05$, Table 1).

Table 2. Mean Centering ratio (mean \pm SD)

Level \ Group	Group 1 (KF)	Group 2 (PF)	Group 3 (PT)	Group 4 (K3)
1 mm	0.17 \pm 0.06 ^a	0.22 \pm 0.05 ^a	0.34 \pm 0.07 ^b	0.21 \pm 0.03 ^a
3 mm	0.16 \pm 0.08 ^a	0.18 \pm 0.11 ^a	0.15 \pm 0.04 ^a	0.21 \pm 0.03 ^a
5 mm	0.19 \pm 0.11 ^a	0.15 \pm 0.06 ^a	0.45 \pm 0.06 ^b	0.29 \pm 0.04 ^a
7 mm	0.15 \pm 0.04 ^a	0.31 \pm 0.10 ^b	0.44 \pm 0.06 ^{ab}	0.48 \pm 0.07 ^{ab}

^{a,b}: Groups identified by different alphabets are significantly different in horizontal row ($p < 0.05$). Groups identified by same alphabets are not significantly different in horizontal row ($p > 0.05$).

Centering ratio

In all groups, centering ratio showed the lowest value at 3 mm level. And except at 3 mm level, there was a tendency of Group 3 (PT) to remain less centered in the canal than other groups ($p < 0.05$, Table 2).

IV. Discussion

A number of techniques are currently available to evaluate the efficacy of instruments to remain centered during root canal preparation. Conventional analytical methods may employ reassembly techniques⁹⁾, which evaluate cross-sections of root canals before and after preparation. This technique causes some loss of root material because of the thickness and lateral movement of the band saw. Furthermore, some oblique-sectioned surfaces in curved canals could act as ledges that hinder the file from advancing to the working length. Another method, the micro-computed tomography, is emerging in several endodontic research facilities as a nondestructive and accurate method to analyze canal geometry and the relative effects of shaping instruments or techniques¹⁰⁾. This innovation was achieved because new hardware and software was available to evaluate the metrical data created by micro-computed tomography, thus allowing geometrical changes in prepared canals to be determined in more detail¹¹⁾. In the present study, using micro-computed tomography, we compared cutting ability

and centering ability of various endodontic file systems by calculating the amount of dentin removed and centering ratio, respectively.

The amount of canal volume change was least in Group 1 (KF), followed in increasing order by Group 2 (PF), Group 4 (K3), and Group 3 (PT). Group 3 (PT) and Group 4 (K3) showed almost same results. It assumed that K3 and ProTaper systems have excellent cutting efficiency during instrumentation.

The centering ratio can define the ability of instruments to remain centered in shaped canals. This experiment used a centering ratio formula to evaluate canal transportation. According to this formula, centering ratio approaches zero as T' and T become closer. In the current investigation, all instrumentation systems produced some canal transportation. Especially, ProTaper system made more transportation than other systems except at 3mm level and tended to transport towards the furcation at 5 mm and 7 mm levels.

There are several studies that their findings are consistent with the findings of this experiment. ProTaper removed more canal wall and lessened the canal curvature than did the other instruments¹²⁾. Bergmans *et al.*¹³⁾ reported that the maximum centering ratio was 0.47 for ProTaper system and 0.27 for K3 system, despite of no significant differences between two groups and a center displacement towards the furcation at the coronal section was demonstrated. In this study, centering ratio of K3 and PT system was 0.29 ± 0.04 and 0.45 ± 0.06 at 5 mm level that were sim-

ilar as the Bergmans *et al.*'s results. The centering ratio of the Ni-Ti rotary instruments was largest at the 7 mm level and smallest at the 3 mm level in this study, so canal transportation would be larger at the coronal region than at the apical region. The finding of canal transportation was consistent with previous work of Peters *et al.*¹⁴⁾ that canal transportation was prominent at the coronal region in mesiobuccal canals of maxillary molars with significant differences.

Ni-Ti rotary instruments are characterized by different cross-sections and designs of blades. One of the latest trends in NiTi rotary shaft design is the introduction of a radial land relief in combination with a positive rake angle (K3 from SybronEndo). This asymmetrical, more aggressive file design should allow better debris removal, and a cutting rather than a planning action which differs from those possessing U-shaped blades with radial land areas such as ProFile¹⁵⁾. It is well known that although there are several factors affecting the cutting efficiency of NiTi rotary systems, the rake angle of the cutting blade plays a central role¹⁵⁾. Since dentin is a dense and resilient material, instruments having a negative rake angle are less efficient and require more energy to cut dentin than files with a neutral or positive rake angle¹⁶⁾.

A unique feature of the shaping files in ProTaper system is their progressively tapered design, which clinically serves to significantly improve flexibility and cutting efficiency; it typically reduces the number of recapitulations needed to achieve length, especially in tight or more curved canals¹⁷⁾. And ProTaper has a convex triangular cross-sectional design. This feature reduces the contact area between the blade of the file and dentin, and serves to enhance the cutting action and improve safety by decreasing the torsional load¹⁸⁾. In this study, more aggressive dentin cutting of Protaper resulted in large canal transportation despite of following clinical guidelines suggested by Ruddle¹⁸⁾. It may be that as in the present study, the higher values of centering ratio for ProTaper resulted from the absence of

radial land area in combination with the large coronal diameter of the ProTaper-shaft¹³⁾.

In several studies, the shaping ability of different rotary Ni-Ti instruments and stainless steel hand K-files has been compared. In severely curved simulated canals the use of different rotary Ni-Ti instruments such as ProFiles¹⁹⁾, GT files²⁰⁾, and K3 instruments²¹⁾ resulted in less canal transportation compared with stainless steel K-Flexofiles. The present investigation does not corroborate the findings of previous studies. However, Stone *et al.*²²⁾ found that rotary NiTi instrumentation transported the canal more than hand instrumentation. Esposito and Cunningham²³⁾ found that NiTi files were more effective than stainless steel files in maintaining the original canal path of curved root canals when the apical preparation was enlarged beyond size 30.

There are many factors affecting the results. Evidence suggests that canal anatomy influences preparation outcomes; significantly more aberrations are recorded when preparing simulated canals with more acute curves in plastic blocks using Ni-Ti rotary instruments²⁴⁾. In addition, three-dimensional analysis using micro CT indicated that canal transportation was more pronounced when shaping narrow curved canals than wider specimens²⁵⁾. Further research is needed to evaluate the characteristics of Ni-Ti rotary systems to determine whether they can be used safely and efficiently in canal shaping procedure.

V. Conclusions

In this study, we compared the centering abilities of four root canal instrument systems and the amounts of dentin removed after final instrumentation using them.

ProTaper system has a tendency to remove more dentin and to transport the original canal towards the furcation more than K-Flexofile, ProFile, K3 system. Further studies will be needed to evaluate the characteristics of each file system in other aspects including three-dimensional analysis of the prepared canal.

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국문초록

방사선 미세컴퓨터단층촬영을 이용한 네 종류 file systems의 중심유지능에 관한 비교

고혜숙 · 유현미 · 박동성*

성균관대학교 의과대학 삼성서울병원 치과보존과

이 연구의 목적은 네 종류 file systems의 중심유지능과 근관성형 전후의 상아질 삭제량을 비교하는 것이다.

10-20도의 만곡을 갖는 발거된 20개의 하악 제1대구치의 근심근관(총 40개의 근관)을 근관성형 전에 X선 미세 단층촬영 스캐너를 이용하여 스캔하였다. 제 1군은 근관부를 넓힌 후 stainless steel K-Flexofile을 사용하여 step-back technique으로 근관성형하였고, 나머지 군들은 각 제조사의 추천대로 ProFile system (2군), ProTaper system (3군), K3 system (4군)을 사용하여 crown-down technique으로 근관성형하였다. 모든 근관의 근단부 기구조작은 #25 크기까지 시행하였고 근관성형 후 스캔하였다. 3차원 영상 소프트웨어로 근관성형 전후의 스캔된 이미지들을 재구성하여 근관의 전체적 부피 변화를 측정하였다. 또한, 근단공으로부터 1, 3, 5, 7 mm 되는 지점의 근관 횡단면을 비교하여 근관성형 전후의 단면적 변화와 중심변위율을 산출하였다.

그 결과, ProTaper와 K3가 다른 file systems보다 상아질을 더 많이 삭제하는 경향을 보였고 모든 실험군에서 중심변위율은 근단공으로부터 3 mm 지점에서 가장 낮은 수치를 나타냈으며, 3 mm 지점을 제외하고는 ProTaper가 다른 file systems보다 중심유지능이 떨어지는 결과를 얻을 수 있었다 ($P < 0.05$).

주요어: X선 미세단층촬영, ProFile, Protaper, K3, 중심변위율, 3차원 영상 소프트웨어