



A Liner Breakage in Total Hip Arthroplasty after Using 1st Generation Highly Cross Linked Polyethylene Mated against 36-mm Metal Head: A Case Report

Won-Kee Choi, MD, Myung-Rae Cho, MD, Seung-Bum Chae, MD, Dong-Young Kim, MD

Department of Orthopaedic Surgery, Daegu Catholic University College of Medicine, Daegu, Korea

It has been known the highly cross linked polyethylene (HXLPE) has an advantage of improved wear rate. However, the alteration in mechanical properties such as decreased tensile yield and fatigue strength make concerns about fragility of HXLPE. We experienced a case of HXLPE breakage. But, this case of liner breakage happened although patient belonged to normal BMI and proper acetabular cup position so called “safe zone” on radiographs. So, we report this case with reference review.

Key Words: Highly cross linked polyethylene, Wear, Fragility

There are many advantages in using 36-mm femoral head mated with highly cross linked polyethylene (HXLPE) as bearing surface of total hip arthroplasty. A larger femoral head has many potential advantages such as stability and increased range of motion, which reduces the risk of impingement and dislocation¹⁾. But, the larger metal head size against polyethylene hip arthroplasty has historically been limited due to concerns regarding increased volumetric wear rates²⁾.

This issue could be addressed with the advent of HXLPE. It has been shown that HXLPE wear rates decreased by 58% to 74% over the ultra high molecular weight polyethylene (UHMWPE) in various *in vitro* studies³⁾. The improvements in stability and observations of lower wear rates with large heads on HXLPE compared to a 28-mm head on standard polyethylene have led to the increased acceptance of 36-mm femoral head mated with HXLPE⁴⁾. But, there are also some trade-offs in using 36-mm femoral head mated with HXLPE. This highly cross linking is made by exposures of gamma radiation. Unfortunately, the increase in gamma dose is associated with the degradations of other mechanical properties including a decrease in tensile yield strength and fatigue strength and resultant liner breakage⁵⁾.

There are few reports of 1st generation HXLPE breakage⁶⁾. Majority of these reports pointed out high body mass index (BMI), improper acetabular cup position, thin liner thickness and impingement between femoral stem and liner, etc. as causes of liner breakage. This case of liner breakage happened although patient

Submitted: June 25, 2015 **1st revision:** August 3, 2015

Final acceptance: August 25, 2015

Address reprint request to

Myung-Rae Cho, MD

Department of Orthopaedic Surgery, Daegu Catholic University Medical Center, 33 Duryugongwon-ro 17-gil, Nam-gu, Daegu 42472, Korea

TEL: +82-53-650-4277 **FAX:** +82-53-652-4272

E-mail: cmr0426@cu.ac.kr

This is an Open Access article distributed under the terms of the Creative Commons Attribution Non-Commercial License (<http://creativecommons.org/licenses/by-nc/4.0>) which permits unrestricted non-commercial use, distribution, and reproduction in any medium, provided the original work is properly cited.

belonged to normal BMI and proper acetabular cup position so called “safe zone” on radiographs.

This paper’s aim is to report HXLPE breakage case of patient operated with 36-mm femoral head coupled with HXLPE and discuss about causes of breakage.

CASE REPORT

A male patient aged 58 years visited our hospital because of right hip joint pain. In the past, he underwent bipolar hemiarthroplasty on the right hip due to osteonecrosis of femoral head 11 years ago and total hip arthroplasty on left hip due to same disease 3 years ago. The patient weighted 52 kg and had BMI of 19.6 kg/m².

On plain film, there was stem loosening at right bipolar hemiarthroplasty. So, we decided to revise the right hip. In 2005, we revised with 54-mm acetabular cup (Trilogy; Zimmer, Warsaw, IN, USA) and 36-mm metal head mated against HXLPE (Longevity; Zimmer) as bearing surface. As to a femoral stem, we revised with 11 mm beaded full coating, non-cemented revision femoral stem (Versys; Zimmer). Post-operative radiograph showed a cup abduction angle of 50° and 23.4° anteversion respectively (Fig. 1). After 10 days since index operation, patient took a weight-bearing within the limits of tolerance, and discharged without any event. After 6 years since 1st revision, the patient

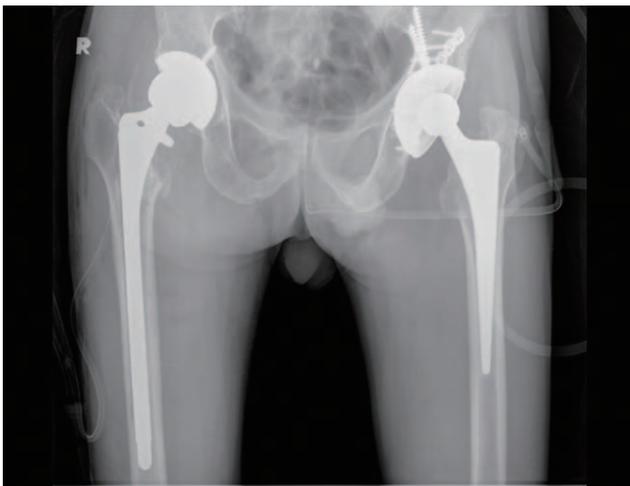


Fig. 1. We conducted 1st revision with 36-mm metal head mated with highly cross linked polyethylene (Longevity; Zimmer, Warsaw, IN, USA) as bearing surface with 54-mm acetabular cup.



Fig. 2. Radiograph demonstrated eccentric femoral head position within acetabular cup, and radiopacity suggesting tines of the locking mechanism (arrow).

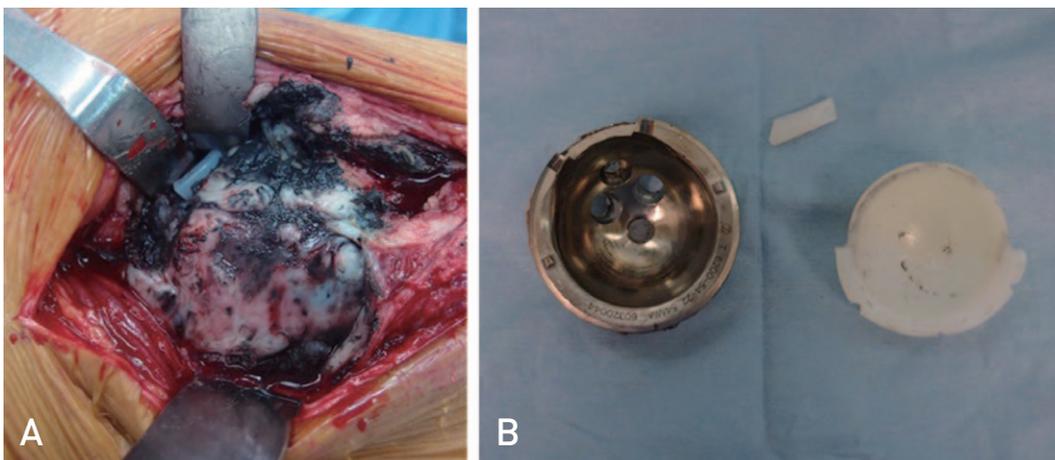


Fig. 3. We found a metallosis, liner fragment (A), and a rim breakage of the Longevity liner (Zimmer, Warsaw, IN, USA) at the superior quadrant (B).

visited our center complaining an abrupt right hip pain developed without recent trauma history. Radiographs demonstrated eccentric femoral head position within acetabular cup and radiopacity suggesting tines of the locking mechanism on the infero-medial side of right hip joint (Fig. 2). On the basis of this finding, we suspected a liner breakage. In the 2nd revision, we identified metallosis (Fig. 3A). Also, we found a fragmentation of the Longevity liner at the superior quadrant (Fig. 3B), severe scratch damages in just below the neck portion of femoral stem and superior quadrant area of liner. After checking stable fixation status of femoral stem, and no damages in Morse taper of femoral stem, we conducted 2nd revision with 56-mm acetabular cup (Trilogy) and 36-mm metal head mated with HXLPE (Longevity) as bearing surface remaining femoral stem. Since leaving the hospital, there have not been special events.

DISCUSSION

There are some risk factors as known as making a HXLPE fracture. Thin liner thickness, impingement between femoral stem and liner, inadequate acetabular cup position, excessive patient's BMI, and excessive patient's motions are being suspected as risk factors of liner breakage⁶⁻⁸. In this case, 1st revision radiographs showed acetabular cup position was in the adequate position so called "safe zone". Also, patient's BMI belonged to normal area.

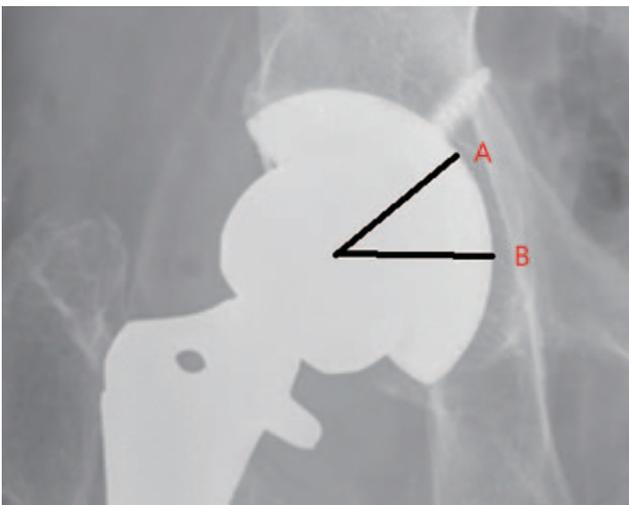


Fig. 4. A line: thickness of highly cross linked polyethylene (HXLPE) was 6.7 mm at pole. B line: thickness of HXLPE was 5.8 mm at 45° angle direction.

Possible hypothesis contributing liner breakage in our case were thin liner thickness, the increased brittleness of HXLPE due to remelting process, and impingement between liner rim and femoral stem. It is important to note that modular liner thickness is often specified on the basis of the nominal material thickness at the specific degree angle of the liner. First revision was conducted with 54-mm acetabular cup. Liner thickness when using 36-mm metal head coupled with HXLPE (Longevity) as bearing surface with 54-mm acetabular cup are 5.8 mm at 45° angle direction and 6.7 mm at pole respectively (Fig. 4). This thickness is the thinnest thing we can use when using 36-mm metal head. But the dimension of edge of liner is less than 5.8 mm. US Food and Drug Administration is approving of at least 3-mm HXLPE application. But, many hip simulator study demonstrated thinner polyethylene components showed that higher contact stress and wear rates². In a study of Berry et al.⁹, 10 cases of catastrophic acetabular liner failure were described. All failures occurred in patients who had acetabular liners implanted with thicknesses of less than 5 mm. So, we conducted 2nd revision with 56-mm acetabular cup to use thicker liner. Liner thickness when using 36-mm metal head coupled with HXLPE (Longevity) as bearing surface with 56-mm acetabular cup are 6.9 mm at 45° angle direction and 7.8 mm at pole respectively.

This manufacture adopts a remelting method to remove remaining free radical. This method degraded mechanical properties, particularly the fatigue strength¹⁰. So, this liner may be vulnerable to crack formation due to impingement. In our case, we found superior quadrant liner rim fracture, and severe scratch damage in just below femoral neck portion as the counter-part of impingement.

On the basis of this findings, we speculate multiple factors including thin liner thickness, impingement between liner rim and femoral stem, and re-melting method to remove remaining free radical involved in HXLPE breakage of this case.

In conclusion, surgeon had better use thicker liner when it is possible and should avoid impingement between liner rim and femoral stem.

REFERENCES

1. Soong M, Rubash HE, Macaulay W. *Dislocation after total hip arthroplasty. J Am Acad Orthop Surg. 2004;12:314-21.*
2. Johnson AJ, Loving L, Herrera L, Delanois RE, Wang A,

- Mont MA. *Short-term wear evaluation of thin acetabular liners on 36-mm femoral heads. Clin Orthop Relat Res.* 2014;472:624-9.
3. Lee JH, Lee BW, Lee BJ, Kim SY. *Midterm results of primary total hip arthroplasty using highly cross-linked polyethylene: minimum 7-year follow-up study. J Arthroplasty.* 2011;26:1014-9.
 4. Harris WH, Muratoglu OK. *A review of current cross-linked polyethylenes used in total joint arthroplasty. Clin Orthop Relat Res.* 2005;(430):46-52.
 5. Pruitt LA. *Deformation, yielding, fracture and fatigue behavior of conventional and highly cross-linked ultra high molecular weight polyethylene. Biomaterials.* 2005; 26:905-15.
 6. Tower SS, Currier JH, Currier BH, Lyford KA, Van Citters DW, Mayor MB. *Rim cracking of the cross-linked longevity polyethylene acetabular liner after total hip arthroplasty. J Bone Joint Surg Am.* 2007;89:2212-7.
 7. Waewsawangwong W, Goodman SB. *Unexpected failure of highly cross-linked polyethylene acetabular liner. J Arthroplasty.* 2012;27:323.e1-4.
 8. Moore KD, Beck PR, Petersen DW, Cuckler JM, Lemons JE, Eberhardt AW. *Early failure of a cross-linked polyethylene acetabular liner. A case report. J Bone Joint Surg Am.* 2008; 90:2499-504.
 9. Berry DJ, Barnes CL, Scott RD, Cabanela ME, Poss R. *Catastrophic failure of the polyethylene liner of uncemented acetabular components. J Bone Joint Surg Br.* 1994;76: 575-8.
 10. Puértolas JA, Medel FJ, Cegoñino J, Gomez-Barrena E, Ríos R. *Influence of the remelting process on the fatigue behavior of electron beam irradiated UHMWPE. J Biomed Mater Res B Appl Biomater.* 2006;76:346-53.